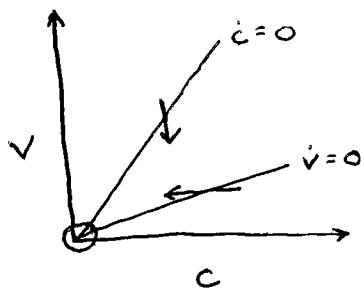
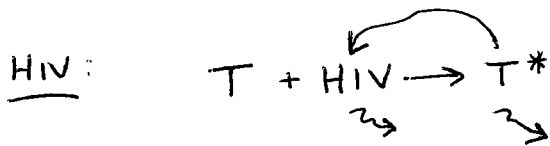


# Lecture 3 : Multistability

- Null clines and cooperativity
- multiple steady-states
- positive feedback revisited
- irreversible transitions
- bistability and noise
- cross repression

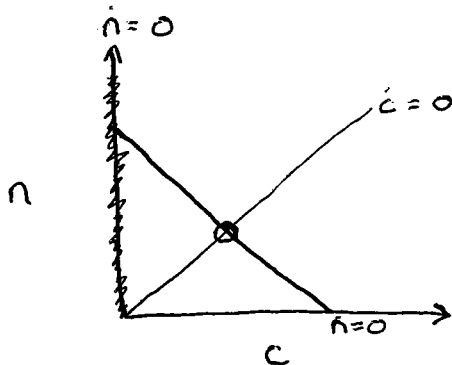
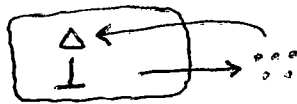
Recap: the intersection of null clines are the steady-states of the system



$$\frac{dc}{dt} = \theta v - c$$

$$\frac{dv}{dt} = Nc - Kv$$

cell-cell:

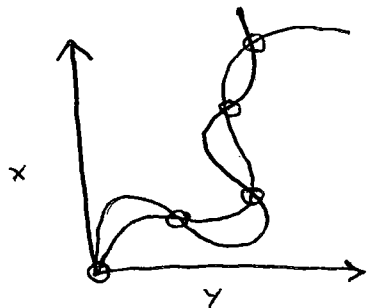


$$\frac{dn}{dt} = Kn(1-n) - Scn$$

$$\frac{dc}{dt} = \theta n - c$$

What has to happen to have multiple steady-states?

Null clines have to intersect at multiple points



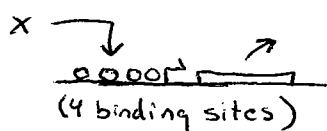
Each intersection is a steady state (stable or unstable)  
 Multistability usually refers to multiple steady states

What types of equations curve?  $\Rightarrow$  polynomials

(or when there is a null cline @  $x=0$  or  $y=0$ )

In biology, polynomial null clines usually arise from cooperativity

examples:

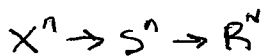


$$\frac{K_4 x^4}{1 + K_4 x^4 + K_3 x^3 + K_2 x^2 + K_1 x}$$

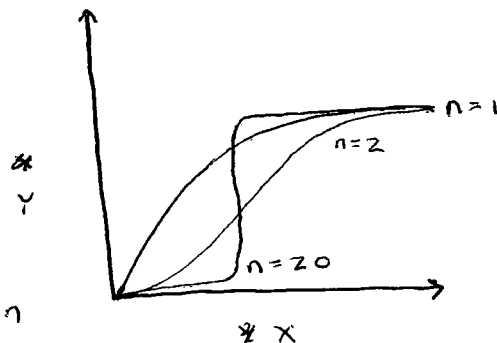
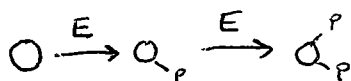
multi-site phosphorylation

(Ken: binding polynomials)

cascades:



m steps  
 cooperativity  
 $n \times m$



$$y = \frac{x^n}{1+x^n}$$

### Competition Models:

eg, sheep/rabbits, lions/lyenas, etc  
two competing species for limited resources  
competitive edge

$$\frac{dX}{dt} = \underbrace{k_x X}_{\text{growth}} \left( 1 - \underbrace{\frac{X}{N_1} - a \frac{Y}{N_1}}_{\text{carrying capacity}} \right)$$

$$\frac{dY}{dt} = k_y Y \left( 1 - \frac{Y}{N_2} - b \frac{X}{N_2} \right)$$

$$\tau \equiv t \cdot k_x \quad x \equiv \frac{X}{N_1} \quad y \equiv \frac{Y}{N_2} \quad K \equiv \frac{k_y}{k_x} \quad \alpha \equiv a \frac{N_2}{N_1} \quad \beta \equiv b \frac{N_1}{N_2}$$

$$\frac{dx}{d\tau} = x(1-x-\alpha y)$$

$$\frac{dy}{d\tau} = y(1-y-\beta x)$$

**K = 1**  
**~~α = 2~~ α = 2**  
**~~β = 2~~ β = 2**

@ steady-state,

$$0 = x(1-x-\alpha y)$$

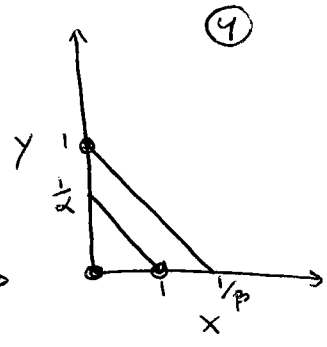
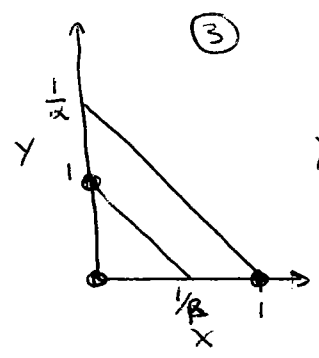
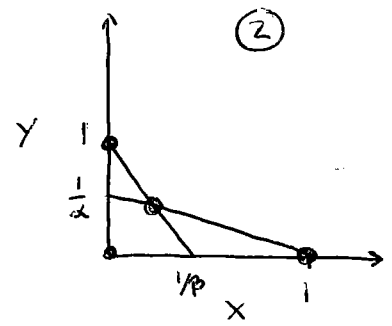
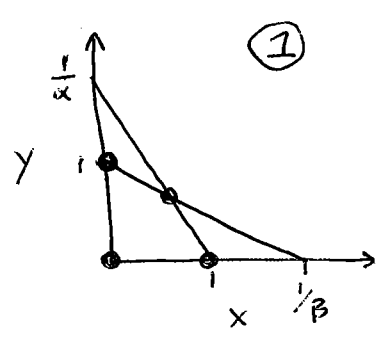
$$0 = ky(1-y-\beta x)$$

null clines at  $x=0$  and  $y=0$

$$0 = 1-x-\alpha y \quad y_1 = \frac{1-x}{\alpha}$$

$$0 = 1-y-\beta x \quad y_2 = 1-\beta x$$

four possibilities based on the values of  $x$  and  $y$



4 steady-states

$$(0,0) \quad (1,0) \quad (0,1)$$

$$y_1 = y_2$$

$$\frac{1-x}{\alpha} = 1-\beta x$$

$$1-x = \alpha - \alpha\beta x$$

$$1-\alpha = x - \alpha\beta x \quad \left( x = \frac{1-\alpha}{1-\alpha\beta} \quad y = \frac{1-\beta}{1-\alpha\beta} \right)$$

Stabilities

$$J = \begin{bmatrix} 1-2x-\alpha y & -\alpha x \\ -\beta y & 1-2y-\beta x \end{bmatrix}$$

@ (0,0)  $J = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$   $\tau = 1+1 > 0$  always unstable

@ (1,0)  $J = \begin{bmatrix} -1 & -\alpha \\ 0 & 1-\beta \end{bmatrix}$   $\tau = -1 - \beta$   
 $\Delta = \beta - 1 > 0$   
 stable when  $\beta > 1$

@ (0,1)  $J = \begin{bmatrix} 1-\alpha & 0 \\ -\beta & -1 \end{bmatrix}$   $\tau = -\alpha$   
 $\Delta = \alpha - 1 > 0$   
 stable when  $\alpha > 1$

@  $\left( x = \frac{1-\alpha}{1-\alpha\beta}, y = \frac{1-\beta}{1-\alpha\beta} \right)$

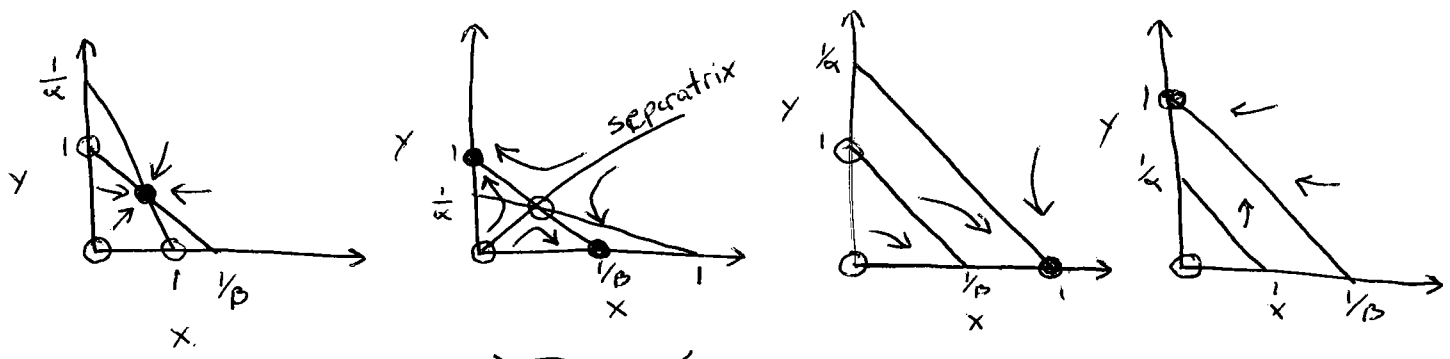
$$\tau = 1 - 2\left(\frac{1-\alpha}{1-\alpha\beta}\right) - \alpha\left(\frac{1-\beta}{1-\alpha\beta}\right) + 1 - 2\left(\frac{1-\beta}{1-\alpha\beta}\right) - \beta\left(\frac{1-\alpha}{1-\alpha\beta}\right)$$

$$= \frac{1 - \alpha\beta - 2 + 2\alpha - \alpha + \alpha\beta + 1 - \alpha\beta - 2 + 2\beta - \beta + \alpha\beta}{1 - \alpha\beta}$$

$$= \frac{\alpha + \beta - 2}{1 - \alpha\beta} < 0 \quad \text{stable when } \alpha + \beta > 2$$

# Complete phase plane

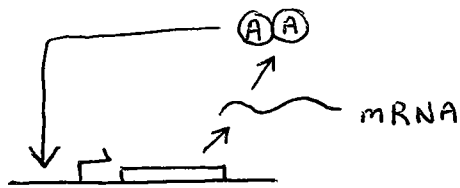
● = stable    ○ = unstable



multistability  
 (initial condition matters)

- A change in parameters or a random perturbation can cause the system to switch between states
- ~~likely~~ Two species sharing some resources are unlikely to coexist
- stable  $\Rightarrow$  1 goes extinct  $\Rightarrow$  climate change  $\Rightarrow$  other species walks in on the system switches to a new state

# Positive feedback revisited



$$\frac{dM}{dt} = \beta_M \frac{KA^2}{1+KA^2} - \gamma_M M$$

$$\frac{dA}{dt} = \beta_A M - \gamma_A A$$

$$\tau \equiv \tau \cdot \beta_A$$

$$m \equiv M\sqrt{K}$$

$$a \equiv A\sqrt{K}$$

$$\frac{dm}{d\tau} = \frac{ba^2}{1+a^2} - gm$$

$$\frac{da}{d\tau} = m - \theta a$$

$$b \equiv \frac{\beta_M \sqrt{K}}{\beta_A}$$

$$g \equiv \frac{\gamma_M}{\beta_A}$$

$$\theta \equiv \frac{\gamma_A}{\beta_A}$$

nullcline 1 :  $m = \left(\frac{b}{g}\right) \left(\frac{a^2}{1+a^2}\right)$

nullcline 2 :  $m = \theta a$

Steady-state solutions

$$\theta a = \left(\frac{b}{g}\right) \left(\frac{a^2}{1+a^2}\right)$$

$$g\theta a(1+a^2) = ba^2$$

$$g\theta a^3 - ba^2 + g\theta a = 0$$

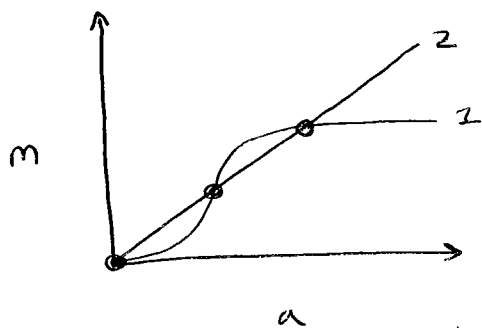
$$a_1 = 0$$

$$g\theta a^2 - ba + g\theta = 0$$

$$a_2 = \frac{b - \sqrt{b^2 - 4g^2\theta^2}}{2g\theta}$$

$$a_3 = \frac{b + \sqrt{b^2 - 4g^2\theta^2}}{2g\theta}$$

(the math in this business is often a polynomial root solving game)

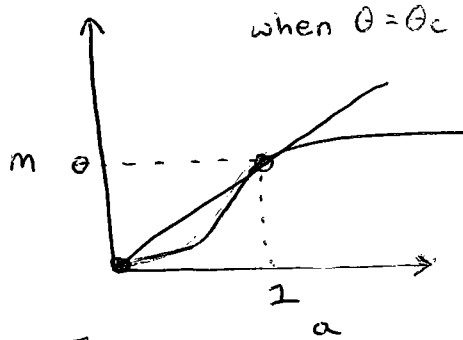


roots  $a_2$  and  $a_3$  are equal when:

$$b^2 - 4g^2\theta^2 = 0$$

$$b = 2g\theta$$

$$\theta_c = \frac{b}{2g}$$



$$a_1 = a_2 = \frac{b}{2g\theta} = \frac{b}{2g(\frac{b}{2g})} = 1$$

$$m_1 = m_2 = \theta$$

calculate stabilities

$$J = \begin{bmatrix} -g & \frac{2ba}{(1+a^2)^2} \\ 1 & -\theta \end{bmatrix}$$

$\tau = -g - \theta$  (always negative)  
 stability determined by

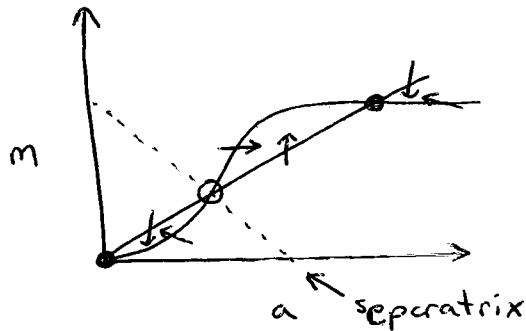
$$\Delta = g\theta - \frac{2ba}{(1+a^2)^2}$$

when  $\theta = \theta_c$

$$\Delta = \frac{b}{2} - \frac{2b}{(1+1)^2} = 0$$

$$a > 1 \quad \Delta > 0 \quad (\text{stable})$$

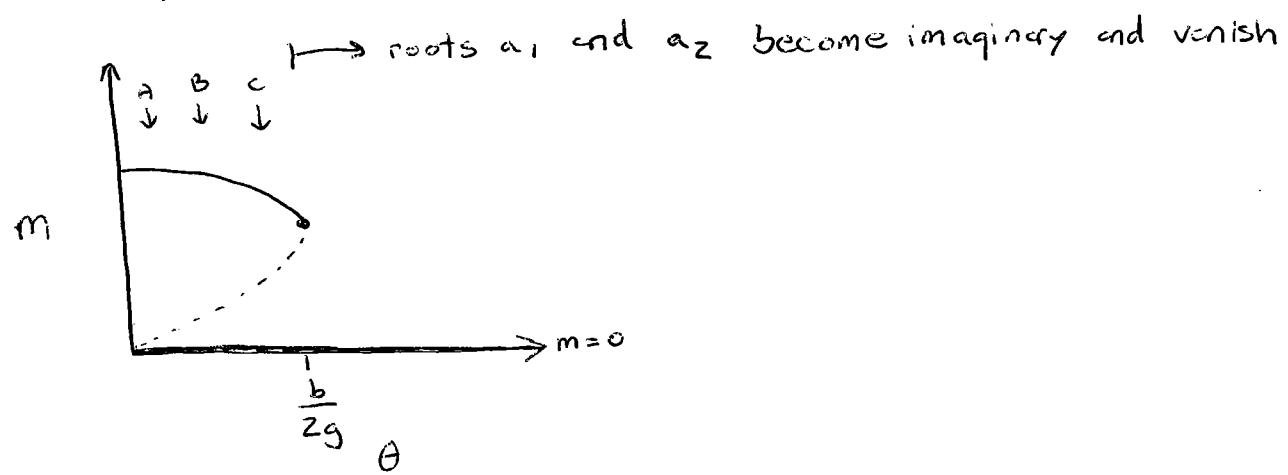
$$a < 1 \quad \Delta < 0 \quad (\text{saddle-unstable})$$



~~Can redraw this as a bifurcation:~~

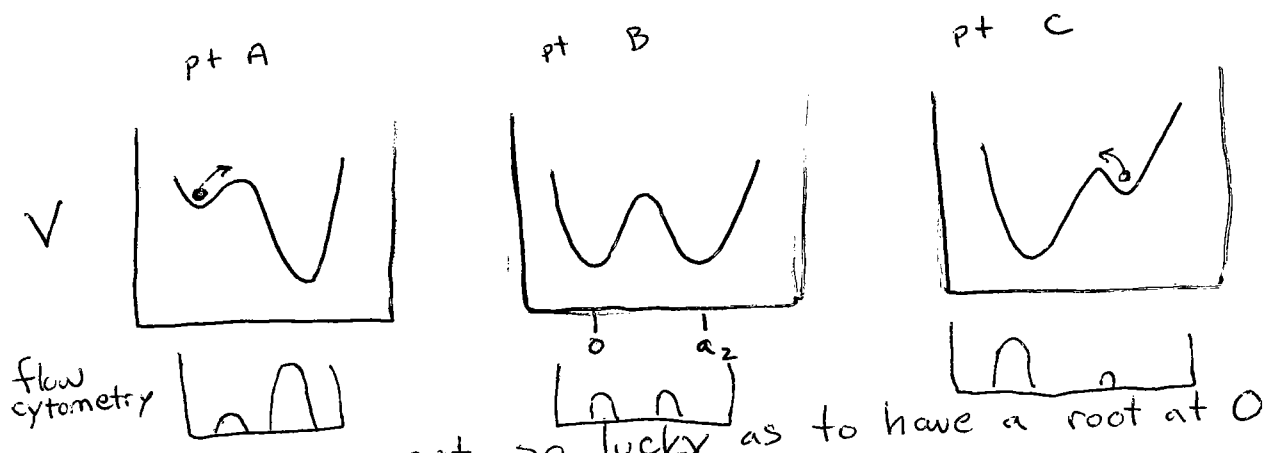
Can redraw as bifurcation diagram

(changes in stability or behavior as a function of a parameter)

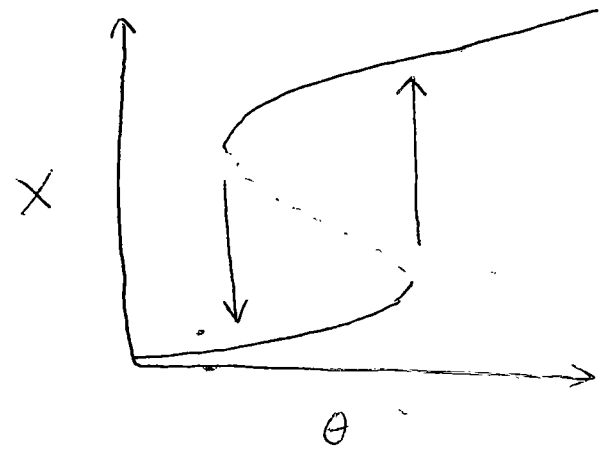


- discontinuous transition
- hysteresis
- stability to noise

Energy diagrams



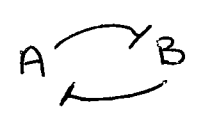
when: you are not so lucky as to have a root at 0





# 2 more ways to get bistability

## cross repression



intuition: 2 steady-states  
 HIGH A, HIGH B  
 LOW B, LOW A

~~$$\frac{da}{dt} = \dots$$~~

$$\frac{da}{dt} = \frac{1}{1+Kb^2} - a$$

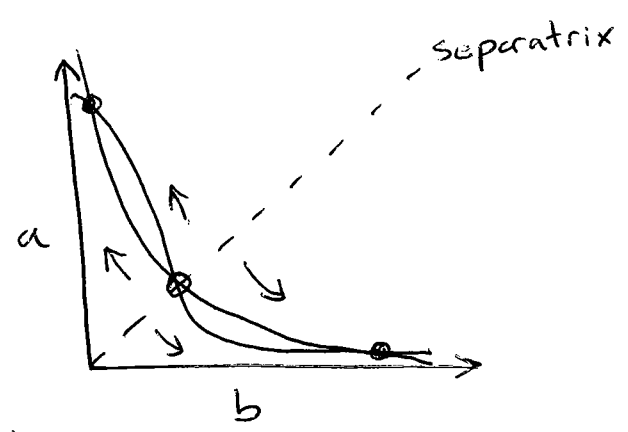
~~$$\frac{db}{dt} = \dots$$~~

$$\frac{db}{dt} = \frac{\beta}{1+Ka^2} - b$$

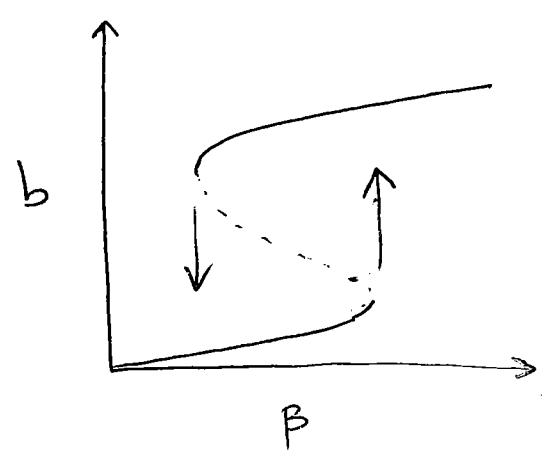
NOTE: still need cooperativity

null lines:

$$a = \frac{1}{1+Kb^2} \quad b = \frac{\beta}{1+Ka^2}$$

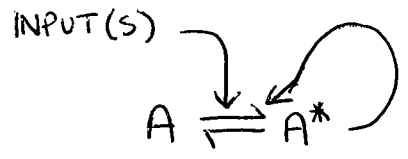


bifurcation diagram



# Bistability w/ perfect Irreversibility

phosphorylation w/ feedback



$$\frac{dA^*}{dt} = S(A_{\text{TOTAL}} - A^*) + f \frac{A^{*n}}{K^n + A^{*n}} - \gamma A^*$$

when  $n > 4$  f large

nullcline:

